

AMENDMENTS THE SPECIFICATION

Please amend the Title on page 1 as follows:

INTERMEDIATE IMAGE TRANSFER ~~TYPE OF~~ DEVICE FOR A COLOR
IMAGE FORMING APPARATUS

Beginning at page 10, line 12, please amend the paragraph as follows:

FIG. 5 is a table listing ~~other~~ with another five intermediate image transfer belts each having a particular amount of surface resistivity variation and image transferability ranks attainable therewith;

Beginning at page 10, line 22, please amend the paragraph as follows:

FIG. 9 is a table listing the amounts of volumetric resistivity variation of ~~other~~ another intermediate image transfer belts and transferability ranks attainable therewith;

Beginning at page 11, line 3, please amend the paragraph as follows:

FIG. 11 is a table listing the amounts of volumetric resistivity variation of ~~other~~ another four intermediate image transfer belts and transferability ranks attainable therewith;

Beginning at page 12, line 4, please amend the paragraph as follows:

FIG. 19 is a table listing showing the presence/absence of image defect estimated on an image with ~~other~~ another nine intermediate image transfer belts different in surface resistivity from each other;

Beginning at page 12, line 8, please amend the paragraph as follows:

FIG. 20 is a graph ~~collecting~~ of experimental results showing stack scattering ranks determined with other six intermediate image transfer belts different in surface resistivity from each other;

Beginning at page 16, line 10, please amend the paragraph as follows:

A fixing unit 25 is positioned beside the secondary image transferring device 22 for fixing the ~~sheet~~ image transferred to the sheet. The fixing unit 25 includes a press roller 27 pressed against an endless fixing belt 26.

Beginning at page 21, line 15, please amend the paragraph as follows:

The variation of resistance increased in five belts in the range of ~~0.55~~ 0.01 $\log \Omega/\square$ to $0.55 \log \Omega/\square$; such five belts were labeled Nos. 1 through 5 in the incrementing order of absolute value. Likewise, the variation of resistance decreased in the other five belts in the range of $0.01 \Omega/\square$ to $0.56 \Omega/\square$; such five belts were labeled Nos. 6 through 10 in incrementing order of absolute value.

Beginning at page 21, line 15, please amend the paragraph as follows:

The variation of resistance increased in five belts in the range of ~~0.55~~ 0.01 $\log \Omega/\square$ to $0.55 \log \Omega/\square$; such five belts were labeled Nos. 1 through 5 in the incrementing order of absolute value. Likewise, the variation of resistance decreased in the other five belts in the range of $0.1 \Omega/\square$ to $0.56 \Omega/\square$; such five belts were labeled Nos. 6 through 10 in incrementing order of absolute value.

Beginning at page 27, line 20, please amend the paragraph as follows:

FIG. 8 shows ~~an~~ a device used to measure the volumetric resistivity of each belt. As shown, while a probe is pressed against one surface of a belt or sample, a preselected voltage of v_2 V is applied via an electrode. In this condition, a current flowing through a counter electrode is measured by an ammeter. For the measurement, use was made of the same high resistance meter and probe as in Example 1. With HYRESTER mentioned earlier, it is possible to freely set a voltage application time t_3 (sec) and to apply a voltage and then ground the electrode 1 for thereby discharging the belt. Further, it is possible to automatically apply the voltage on the elapse of a discharge time t_4 (sec), which is also freely selectable. In addition, the voltage can be repeatedly applied any desired number of times N_2 . There were also used a high-tension power supply COR-A-TROL (610C) and an ammeter Digital Electrometer TR8652 mentioned earlier.

Beginning at page 29, line 14, please amend the paragraph as follows:

FIG. 11 shows transferability ranks in numerical values also determined with the electrophotographic apparatus shown in FIG. 1. Transferability was estimated on the 100,000th image produced by continuing image formation with each of the belts Nos. 16 through 19 whose variations of volumetric resistivity tended to decrease although to different degrees. It is to be noted that the variation of volumetric resistivity is represented by an absolute value. FIG. 12 is a graph showing the results of measurement conducted with the device described with reference to FIG. 8.

Beginning at page 33, line 21, please amend the paragraph as follows:

Hereinafter will be described the belt No. 12 as an example of the belt 10 used for measurement. Carbon black was dispersed in a polyamic acid solution. The resulting dispersion was caused to flow on a metal drum, dried, peeled off in the form of a film, and

then extended at high temperature to form a polyimide film. The polyimide film was cut in a suitable size to thereby produce a seamless belt formed of polyimide resin. Generally, to form a film, after a polymer solution with carbon black dispersed therein has been introduced into a hollow cylindrical mold, the mold is rotated while being heated at 100°C to 200°C to thereby form a film by centrifugal molding. The film thus formed is removed from the ~~fold~~ mold in a half-set condition, put on an iron core, and then subject to polyimide reaction at 300°C to 450°C and fully set thereby.

Beginning at page 34, line 16, please amend the paragraph as follows:

While the illustrative embodiment is implemented as an indirect image transfer type of image forming apparatus shown in FIG. 1, it is similarly applicable to a direct image transfer type of image forming apparatus. FIG. 15 shows a specific configuration of the direct image transfer type of image forming apparatus. As shown, a sheet S is conveyed by ~~the~~ a registration roller pair 49 in synchronism with image formation effected with ~~the~~ drums 40. While a belt conveyor 10' is conveying the sheet S, toner images of different colors are sequentially transferred from the drums 40 to the sheet S one above the other at consecutive image transfer stations 62. As for the rest of the configuration and operation, the image forming apparatus of this type is similar to the indirect image transfer type of image forming apparatus.

Beginning at page 50, line 9, please amend the paragraph as follows:

A method of satisfying the range of the ratio a/b stated above will be described hereinafter. FIG. 27 is a graph showing a relation between a gap G_p for development and the ratio a/b . The gap G_p refers to a distance between the sleeve 60 for depositing toner on the drum 40 and the drum 40. As shown, the gap G_p and ratio a/b have a positive correlation; the

ratio a/b increases with an increase in gap G_p . It is therefore possible to confine the ratio a/b in the range of from 1.0 to 1.4 by adjusting the gap G_p . In the illustrative embodiment, if the gap G_p is between 0.2 mm and 0.4 mm, then the ratio a/b can be confined in the range of from 1.0 to 1.4. This, however, depends on the linear velocity ratio of the sleeve to the drum and other conditions for the developing device as well as on the carrier resistance of a developer. In the illustrative embodiment, the above linear velocity ratio is selected to be 2.0 while use is made of a developer whose carrier resistance is $1 \times 10^{10} \Omega$ lying in the usual range of from $1 \times 10^9 \Omega$ to $1 \times 10^{13} \Omega$.

Beginning at page 51, line 3, please amend the paragraph as follows:

Another method of confining the ratio a/b in the particular range stated above is to adjust the resistance of carrier grains that convey toner grains electrostatically deposited thereon to the drum 40. For example, by lowering the resistance of the carrier grains, it is possible to reduce the strength of an electric field at the contour of an image between the sleeve 50 and the drum 40 and therefore to prevent toner grains from depositing more on the contour than on the other portion of the image. This reduces to a certain degree an occurrence that the line amount becomes larger than the solid amount, thereby limiting the ratio a/b to 1.4 or below.

Beginning at page 64, line 23, please amend the paragraph as follows:

As stated above, the second and third embodiments described above, implemented as an intermediate image transfer type of image forming apparatus each, obviate irregular image transfer otherwise occurring at the time of primary image transfer N1 due to an irregular potential distribution deposited on the intermediate image transfer body at the time of primary image transfer N1 preceding the above image transfer.

Beginning at page 65, line 6, please amend the paragraph as follows:

Further, there can be obviated irregular image transfer otherwise occurring at the time of primary image transfer N1, which follows secondary image transfer N2, due to the potential contrast of the intermediate image transfer body occurred at the time of secondary image transfer N2.